### CONFIDENTIAL

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	INTERIM ENGINEERING REPORT							
	ON							
	VII.							
	TRANSMITTER-RECEIVER PROJECT							
	ASSIGNED							
	REPORT NO. 8							
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	COVERING THE PERIOD							
	NOV. 1, 1953 TO DEC. 31, 1953							
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# SECTION I PURPOSE OF PROJECT

The general purpose of this project is to investigate and develop					
transistor circuitry for use in transmitter-receiver equipment					
Specifically, the object is to determine the electrical 50	X1				
characteristics of suitable types of transistors, to propose new types of					
transistors with desirable electrical characteristics for the transmitter-					
receiver, and to determine the most practical overall circuit configura-					
tion for the transmitter-receiver using transistors wherever possible.					

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### SECTION 11 PROJECT STATUS

Means of stabilizing the operating point of junction transistors have been achieved. Electrical characteristics and noise figure have been measured on available transistors. Life tests have been made. Specific circuits including oscillators, mixers, audio amplifiers, i-f amplifiers, and r-f amplifiers have been studied. A breadboard radio receiver (3 to 6 mc) has been built. High-frequency equivalent circuits for junction transistors have been evolved. A 2 to 8-mc prototype receiver is being built.

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## SECTION III SUMMARY OF PROGRESS THIS PERIOD

(November-December 1953)

- A. Construction and testing of two tuners were completed.
- B. Preliminary tests of a 2-8 mc breadboard receiver using tuner #1 have been made and circuits modified.
- C. Construction of a prototype receiver using tuner #2 is 90% complete.

#### SECTION IV

#### DETAILS OF WORK DONE THIS PERIOD

#### A. TUNER CONSTRUCTION AND TESTING

Two complete tuners have been constructed. Tuner #1 has been used and tested in the breadboard receiver while tuner #2 is being incorporated in the receiver model. Similar coil designs are used in both tuners, but 1-1/4" long cores are used in the #2 tuner while 1" long cores are used for #1 tuner. Comparing the coil data (Table 1) for both tuners, one can see that both the Q of the coils and the frequency coverage at both bands have been improved in tuner #2.

#### B. PRELIMINARY TESTS OF BREADBOARD 2-8 MC TUNABLE RECEIVER

A breadboard 2-8 mc tunable receiver using tuner #1 has been tested and the circuit modified as shown in Figure 1. Circuit modifications and the results of preliminary performance tests will be described briefly as follows. In general, the performance of this breadboard model receiver meets the specifications.

#### 1. TRACKING COIL DESIGN AND TRACKING CURVE

A shunt-inductance tracking circuit is used in the oscillator. The value  $L_T$  of the shunt tracking coil required is calculated from the relation:

$$\frac{\frac{L_{1}L_{T}}{L_{1}+L_{T}}}{\frac{L_{2}L_{T}}{L_{2}+L_{T}}} = \left(\frac{f_{2}}{f_{1}}\right)^{2} \qquad C = \begin{cases} \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{cases}$$

where

 $f_1 = \min$ . frequency of resonance (mc).

 $L_2$  = value of L required to resonate with  $L_T$  and C at  $f_1$  ( $\mu h$ ).

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### TABLE I--TUNER COIL DATA (All data taken with coils in the tuner).

 $f_{max}$  - max. frequency of operation of coil.

 $\textit{C}_{\max}$  - capacitance required to resonate coil with core out at  $f_{\max}.$ 

 $Q_m$  - Q of coil at  $f_{max}$ .

 $f_{min}$  - min. resonant frequency obtainable with coil with core in the coil and resonant with  $C_{max}$ .

frequency ratio =  $\frac{f_{max}}{f}$ 

	T	<del> </del>	Jmin		<del></del>	·				
· .	TUNER #1				TUNER #2					
	f <sub>max</sub>	C <sub>max</sub> μμε	$Q_m$	f <sub>min</sub> mc	$\frac{f_{max}}{f_{min}}$	f <sub>max</sub> me	C <sub>max</sub> μμ <b>ί</b>	$Q_m$	f <sub>min</sub> mc	$\frac{f_{max}}{f_{min}}$
HIGH FREQUENCY COILS										•.
OSCILLATOR	8	135.4	65.5	3.80	2.11	8	134.2	75	3.63	2.20
ANTENNA COUPLER	8	140.2	62.5	3.63	2.20	8	134.0	72	3.74	2.14
R-F INTERSTAGE COUPLER #1	8	136.8	60.5	3.77	2.12	8	134	70	3.62	2.21
R-F INTERSTAGE COUPLER #2	8	130	63	3.75	2.13	8	132.1	73	3.68	2.17
LOW FREQUENCY COILS				. '						
OSCILLATOR	4	132.3	62.5	1.93	2.07	4	136.7	75	1.86	2.15
ANTENNA COUPLER	4	129.7	71.0	1.93	2.07	4	141.0	78	1.87	2.14
R-F INTERSTAGE #1	4	128.0	71.0	1.95	2.05	4	139.5	76	1.89	2.12
R-F INTERSTAGE #2	4	133.3	71.0	1.92	2.08	4	138.7	80	1.82	2.20

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 $f_2$  = max. frequency of resonance (mc).  $L_2$  = value of L required to resonate with  $L_T$  and C at  $f_2$  ( $\mu$ h).

For the high-frequency coil, we have

$$f_1 = 4.455 \text{ mc}$$
  $L_1 = 12 \mu \text{h}$   $f_2 = 8.455 \text{ mc}$   $L_2 = 3 \mu \text{h}$ 

Therefore,

$$L_T = 78 \mu h$$

$$C = 120 \mu \mu h$$

and, for the low frequency coil,

$$f_1$$
 = 2.455 mc  $L_1$  = 48  $\mu$ h  $f_2$  = 4.455 mc  $L_2$  = 12  $\mu$ h Therefore,  $L_T$  = 158  $\mu$ h  $C$  = 112  $\mu\mu$ f

A calibration curve for the high band of the receiver has been obtained as shown in Figure 2. The travel of the tuner is measured in terms of revolution of the tuner shaft (32 revolutions of the tuner shaft is evuivalent to one inch linear travel of the tuner). The linearity is expected to be improved by using tuner #2.

#### 2. OSCILLATOR INJECTION VOLTAGE

Data on oscillator injection voltage to the mixer vs frequency (using the high-frequency-band oscillator of tuner #1) is plotted as Figure 3. Results show that a variation of oscillator injection voltage from 160 mv to 500 mv has been obtained as frequency varies from 4 to 8 mc. This range of magnitude of the injection voltage lies in the reasonable working range where approximately constant conversion gain can be obtained from the mixer (see Report #2 on the transistor mixer). The secondary winding of the high-frequency oscillator coil consists of 7-1/2 turns, evenly spaced between the primary coils, while the low-frequency oscillator coil has 15 turns.

#### 3. AGC PERFORMANCE

Among various methods of applying AGC to the receiver, the method shown in the schematic diagram (Figure 1) best meets the required performance.

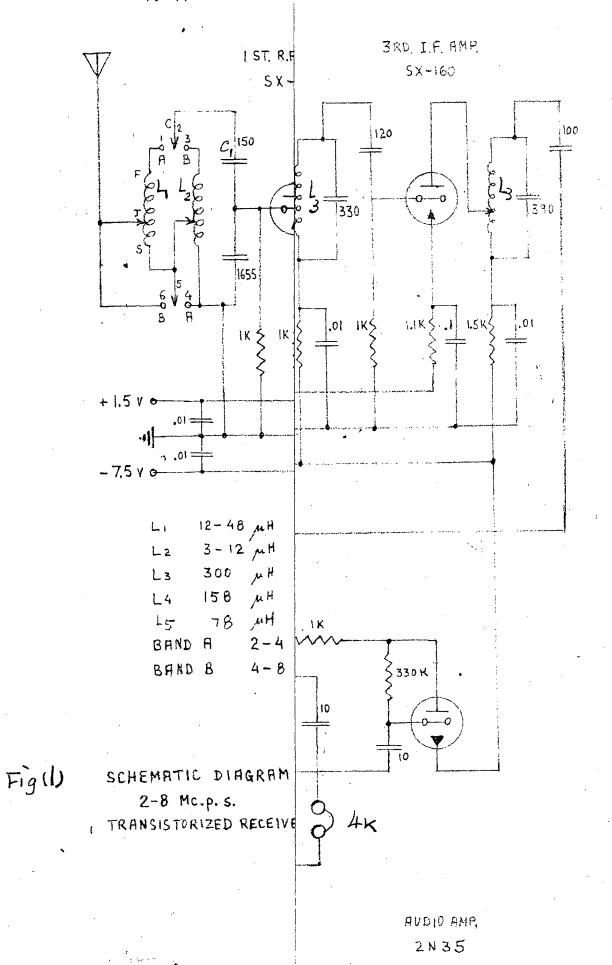
Figure 4 shows the different AGC characteristics that may be obtained. Curve 4 shows the response of audio output versus the r-f input voltage for AGC applied to the first i-f amplifier only. Curves 2, 3, and 4 show the effect of applying AGC to the first and second i-f amplifier simultaneously. A 3-db maximum audio output variation can be obtained for the required variation of input signal from 15  $\mu v$  to 10 mv by using the AGC system with  $R_{d1}$ = 120 ohms and  $R_{d2}$  = 50 ohms (curve 4).

#### 4. PERFORMANCE OF THE RECEIVER

The following data was obtained in the first tests: Sensitivity - 15  $\mu v$  input at 4 mc with a 16 db signal-to-noise ratio. Signal modulated 30% with 400 cycles. 5 mw audio output.

Selectivity - 6-db bandwidth is 13 KC.
60-db bandwidth is 90 KC.

Image Rejection - Better than 40 db (2-8 mc).



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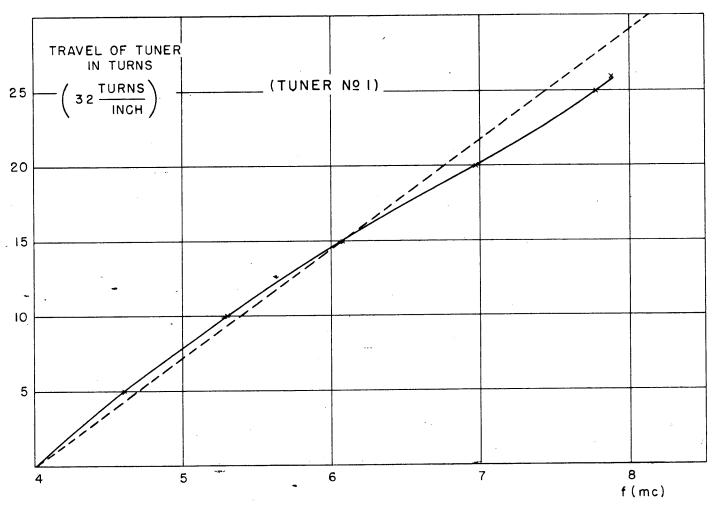


FIG. (2) TUNING CURVE OF HIGH-BAND OF 2-8mc RECEIVER

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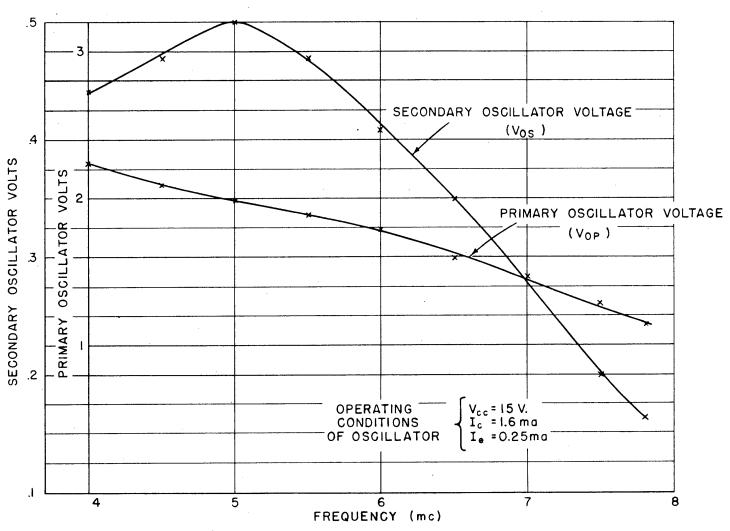
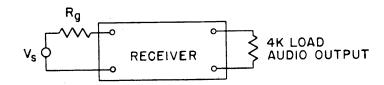
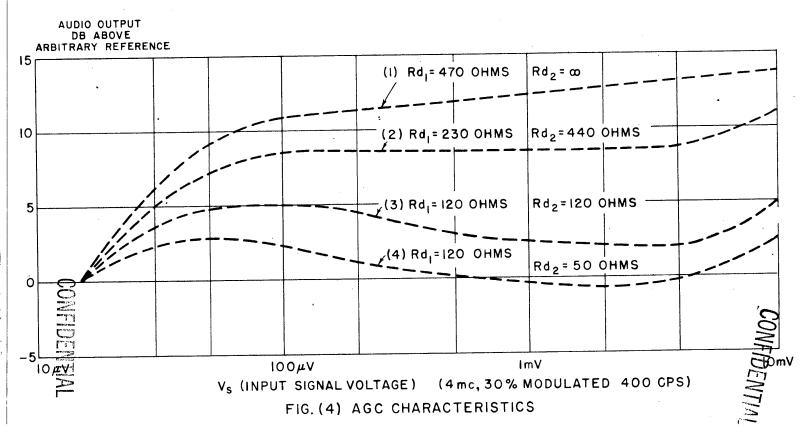


FIG. 3 HIGH FREQUENCY OSCILLATOR INJECTION VOLTAGE VS FREQUENCY

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